Koyo High Wing Series Drive Shafts





JTEKT Koyo TOYODA

CAT.NO.B2022E

High wing series drive shafts that handle all kinds of environment with proven results, technology, research and dev elopment

In order to improve the reliability of our drive shafts under severe conditions, JTEKT has been continuously committed to research and development of technologies, built upon a wealth of results and experiences achieved with our customers over many years.

Our products also have high compatibility through adoption of standard mounting dimensions. This catalogue includes dimension tables for respective model numbers, technical data, handling and failure cases, which we believe will surely help with design of construction machinery and railway rolling stocks. We thank you in advance for your support.

> **JTEKT produc** ts supporting construction machinery and railway rolling stocks

CONTENTS

	Introduction to drive shaft	
	Functions	03
	Appearance and configuration of drive shafts	04
	Efforts to improve reliability	
	Long-interval greasing cross & bearing	05
	Spline seal structure of muddy water resistance improvement	06
	Handling explanation	07
	Cases of failures	08
J	Technical data	
IJ	General characteristics of universal joint	09
	Drive shaft selection	11
	Balance quality of drive shaft	12
	Composition of identification numbers	13
	Torque capacity	14
	Specifications	14
•	Analysis/evaluation equipment	28
	Drive shaft selection sheet	29

JTEKT deals with severe conditions with its No.1 & Only One technologies.

Our drive shafts for construction machinery and railway rolling stocks to meet your needs

Introduction to drive shafts

Functions

A drive shaft is a device to smoothly transmit rotation torque by connecting a driving shaft and a driven shaft that are not aligned on the same axis. Since it has two universal joints on one shaft, it can connect the driving shaft and the driven shaft flexibly.

In addition, one universal joint has four rolling bearings (cross & bearing) that can minimize torque loss with low friction.

Representative applications of drive shaft



• For diesel locomotives





Efforts to improve reliability

1. Long-interval greasing cross & bearing

Features

- (1) Oil seal lip from double to triple, and the optimization of shape and position.
- (2) Reduction of roller contact stress with torque load by length up and crowning optimization
- (3) Abrasion resistance improved by adding glass fiber to thrust washer
- (4) Bearing cup shape reviewed and cost reduced by abolishing the roller washer

Cross & bearing structure



Conventional product: Greasing interval of 250 hours

Thrust washer (PA66+GF)

Abrasion resistance improved by adding glass fiber

Oil seal

Seal lip from double to triple, and the optimization of the shape and position



Roller

Reduction of contact stress by length up and crowning optimization



Product with long-interval greasing: Greasing interval of 2000 - 4000 hours

Evaluation results



2. Spline seal structure of muddy water resistance improvement

Features

Since the cover tube type spline seal has a structure that seals the sleeve (female spline) outer diameter part, (1) It is not necessary to surpass the male spline major diameter by deforming the seal lip at the time of assembly, so a urethane rubber seal with high rigidity can be used.

- (2) The distance from the seal to the spline is long, so muddy water does not reach the spline easily.
- (3) A double cover has been added to protect the seal part, improving endurance further.

Spline seal configuration



Evaluation result of spline muddy water endurance test

Muddy water resistant performance **Greatly** improved





Handling explanation



High wing series features safe and secure torque transmission by a parallel key, and high torque capacity.

The following are the handling method and caution points to ensure that the drive shaft delivers its expected performance.

Handling of drive shaft

Caution points for handling





- (1) Do not hit the cross & bearing part with hard metal so that a shock should be avoided. If it is necessary at the time of assembling, hit it lightly with a non-ferrous metal (copper, etc.) or plastic hammer.
- (2) Tighten the fixing bolts of the bearing cups by setting the bearing cups in the proper positions in the yoke to form an X shape. If you fit the bearing cups with the tightening force of bolts or fix only one bearing cup with the bolt and then set the other, it may cause troubles such as scars on the spigot joint part and attaching surface, and attachment of bearing cups at a slant.
- (3) Never conduct welding between the bolts and the bearing cups and between the yoke and the bearing cups.

(4) Do not disassemble the cross & bearings unless absolutely necessary.

About Iubrication

(1) Greasing interval

It is recommended to apply grease every 2000 - 4000 hours, though it depends on the usage environment.

- (2) Grease to be used Lithium grease with extreme-pressure additive
- (3) Greasing of cross & bearings

Apply grease until it overflows from all of the four shafts of the cross. Wipe off the overflowing grease because dirt may adhere to it.

(4) Greasing of spline part

To apply grease an onboard drive shaft, move the vehicle body so that the spline should be compressed to the minimum. When grease leaks out of the center of the plug attached to the sleeve yoke, greasing is complete.

If the drive shaft is removed from the vehicle because of overhaul, etc., apply grease with the spline compressed to the minimum.



About cross & bearing attaching bolt

(1) Bolt

Use the attached bolt or part for repair specified by JTEKT.

- (2) Torque wrench
- Use a calibrated torque wrench.
- (3) Specified tightening torque
 - Tighten with the specified torque.

Cases of failures

Flaking **Breakage** Flaking has occurred in the raceway surface of rolling Failures example Breakage is caused from the fillet radius part of the neck contact surface of the cross and cup. Failures example of the cross and the fracture surface has no beach mark Cause Brittle fracture due to excessive load Compare the calculated life and the required life and Measure increase the size as necessary Check the usage conditions Measures Increase the size as necessary Breakage is caused from the fillet radius part of the neck The tube has a crack near the border of the tube and Failures example Failures example of the cross, and the fracture surface has a beach mark weld bead Fatigue fracture caused by excessive load applied Fatigue fracture caused by excessive load applied Cause Cause repeatedly repeatedly Check the usage conditions Check the usage conditions Measures Measures Increase the size as necessary Increase the size as necessary The bearing set bolts are broken near the yoke Failures example Failures example Bending near the center of the drive shaft interface Cause Brittle fracture caused by use around the dangerous Cause Bolt fatigue fracture caused by looseness of the bolts rotational speed Measures Decrease the maximum rotational speed. If it is Measure Check that the tightening torque has the specified impossible, reduce the length or increase the tube value size

Technical data 🚹



Single universal joints

The driving shaft and driven shaft intermediated by a universal joint has the following relationship between their rotational angles:

 $\tan \phi_2 = \cos \theta \cdot \tan \phi_1 \cdots (1)$

where ϕ_1 : Rotational angle of driving shaft

 $\phi {\sc 2}$: Rotational angle of driven shaft

 $\theta\,$: Shaft operating angle (Fig. 1)

This means that, even if the rotational speed and torque of the driving shaft are constant, the driven shaft is subject to fluctuation in rotational speed and torque.

The speed ratio between the driving shaft and driven shaft can be obtained by differentiating equation (1) with respect to time (t), where ϕ_1 is by $\omega_1 \cdot t$ and ϕ_2 by $\omega_2 \cdot t$:

$$\frac{\omega_2}{\omega_1} = \frac{\cos\theta}{1-\sin^2\phi_1 \cdot \sin^2\theta} \quad \cdots (2)$$

where $\ \omega$: Rotational angular velocity of driving shaft (rad/s)

 $\omega\,{}^{_2}$: Rotational angular velocity of driven shaft (rad/s)

 $\omega\,{}_2\,/\,\omega\,{}_1$: Angular velocity ratio

Equation (2) can be expressed in diagram form as shown in **Fig. 2**. The maximum value and minimum value of the angular velocity ratio can be expressed as follows:

 $(\omega_2 / \omega_1) \text{ max.} = 1 / \cos \theta \cdot \cdot \cdot \cdot \phi_1 = 90^{\circ}$ $(\omega_2 / \omega_1) \text{ min.} = \cos \theta \cdot \cdot \cdot \cdot \cdot \phi_1 = 0^{\circ}$

The maximum fluctuation rate of angular velocity in a universal joint can be expressed by the following equation:

$$\frac{(\omega 2 \max - \omega 2 \min)}{\omega 1} = \frac{1}{\cos \theta} - \cos \theta$$

The torque ratio between input and output can be expressed by the diagram shown in **Fig. 3**. The maximum value and minimum value can be obtained as shown below, respectively:

> (T_2/T_1) max. = 1/cos θ · · · · ϕ_1 = 0° (T_2/T_1) min. = cos θ · · · · · ϕ_1 = 90°

where T_1 : Input torque T_2 : Output torque

 T_2/T_1 : Torque ratio







Double universal joints

Universal joints are usually installed in pairs. When assembled as shown in **Fig. 4**, that is,

- (1) With equal operating angles in both joints
- (2) Yokes connected to the same shaft in line
- (3) Central lines of all three shafts (driving shaft, intermediate shaft, and driven shaft) in the same plane, the driven shaft rotates exactly in the same way as the driving shaft.

Therefore, they should be attached as shown in the figure on the right as far as possible.





Secondary couple

It is often necessary to consider the secondary couples imposed by universal joints operating at an angle; especially under high angle or large torque. These couples must be taken into account in designing the shafts and supporting bearings.

The secondary couples in the universal joints are in the planes of the yoke. These couples are about the intersection of the shaft axis. They impose a load on the bearings and a bending stress in the shaft connecting the joints, and they fluctuate from maximum to zero every 90° of shaft revolution. The broken lines in **Fig. 5** indicate the effect of these secondary couples on the shafts and bearings.

The equation for maximum secondary couple is as follows:

 $M_1 \max = T \tan \theta$ (for driving shaft) $M_2 \max = T \sin \theta$ (for driven shaft)

where M_1 : Secondary couple on driving shaft $(N \cdot m)$

- M_2 : Secondary couple on driven shaft (N·m)
- T: Driving torque (N · m)
- θ : Shaft operating angle

The ratio of the secondary couple to the driving torque is shown in **Fig. 6**.

The secondary couple M_1 and M_2 can be obtained by multiplying M_1/T or M_2/T by the driving torque T.



Technical data (2)



Drive shaft selection

A drive shaft should be selected so as to satisfy the required strength, service life, operating angle and dimensions necessitated by its purpose. Especially, a drive shaft can be selected if it meets conditions of both strength and life of the universal joint, except for special cases.

Load torque of drive shaft

To decide the size of the drive shaft, it is necessary to grasp the load torque first.

A maximum torque including an impact torque and a mean torque should be known, and it is essential for selecting an appropriate drive shaft to understand the correct maximum torque and mean torque.

Maximum torque:

Value to determine if the strength of each part is sufficient. Mean torque:

Value necessary to calculate the service life

Mean torque

It is apparent that all kinds of machines are not operating thoroughly by their maximum torque. Therefore, if a drive shaft is selected according to a service life calculated from the maximum torque, it results in being uneconomically larger than necessary.

So, it is reasonable to set up a longer expected service life, if the application condition are severe; and shorter, if the conditions are easy.

If, for instance, a job is expressed as in the table below,

Drive stage	1	2	3 · · · · Z
$Torque\left(N\boldsymbol{\cdot}m\right)$	T_1	T_2	$T_3 \cdot \cdot \cdot T_Z$
Rotational (\min^{-1})	n_1	n 2	$n_3 \cdots n_Z$
Time ratio (%)	t_1	t_2	$t_3 \cdots t_Z$

the cube root of mean torque ($T_{\rm m}$) and the arithmetical mean of rotational speed ($n_{\rm m}$) are yielded from the following equations.

$$T_{\rm m} = \sqrt[3]{\frac{(T_1^3 \cdot n_1 \cdot t_1 + \dots T_Z^3 \cdot n_Z \cdot t_Z)}{(n_1 \cdot t_1 + \dots + n_Z \cdot t_Z)}}$$

$$n_{\rm m} = \frac{(n_1 \cdot t_1 + \dots + n_Z \cdot t_Z)}{(t_1 + \dots + t_Z)}$$

Strength of drive shaft

A drive shaft should be selected so that the normal maximum torque shall not exceed the " $T_{\rm D}$ torque." However, it is difficult to determine the true maximum torque, and the engine capacity or motor capacity is used as the maximum torque in many cases, so the safety factor ($f_{\rm S}$) of no less than 1.0 should be considered as the most desirable.

 $f_{\rm S} = T_{\rm D}$ /maximum torque under normal operating conditions > 1.0

The maximum torque that may occur in an emergency should be determined using " T_S torque." The safety factor (f_S) of no less than 1.5 should be considered as desirable in this case as well.

 $f_{\rm S} = T_{\rm S}$ /breaking torque under emergency conditions > 1.5

To select a drive shaft based on a safety factor of 1.5 or less, consult JTEKT as close examination is required in consideration of previous performance records.

Life of drive shaft

There is no worldwide standard for service life calculation of universal joint bearings (cross & bearings) and the service life is calculated according to the unique method developed by each manufacturer. JTEKT employs the following empirical equation based on extensive experimentation (conforming to SAE).

The service life $L_{\rm h}$ is defined as the expected number of operating hours before a flaking occurs on the rolling contact surface of the bearing. The use of the bearings over the service life $L_{\rm h}$ may be practical on a low speed machine.

$$L_{\rm h} = 3000 \ Ke \ \left(\frac{T_{\rm R} \cdot K_{\rm n} \cdot K_{\theta}}{T_{\rm m}}\right)^{2.90}$$

Where, L_h : Average calculated bearing life (h)

- Ke : Experimental correction coefficient (=2)
 - T_{R} : Rated torque (N · m)
 - Tm: Mean torque (N·m)
 - K_n : Speed factor = 10.2/ $n^{0.336}$
 - $K_{ heta}$: Angle factor = 1.46/heta ^{0.344}
 - n: Rotational speed = (min⁻¹)
 - $\theta\,$: Shaft operating angle (°)

Note) A drive shaft should be selected by considering the type of the machine, peripheral equipment, particular operating conditions, and other factors. The method outlined in this catalog is a common rough guide. It is recommended to consult JTEKT for details.

Balance quality of drive shaft

If a rotating drive shaft is unbalanced, it may adversely influence the equipment and ambient conditions, thus posing a problem. JTEKT designs and manufactures drive shafts to satisfy the balance quality requirements specified in JIS B 0905.

Expression of balance quality

The balance quality is expressed by the following equation: Balance quality = $e \omega$

or

Balance quality = en /9.55

where e: Amount of specific unbalance (mm)

This amount is the quotient of the static unbalance of a rigid rotor by the rotor mass. The amount is equal to the deviation of the center of the rotor mass from the center line of the shaft.

- ω : Maximum service angular velocity of the rotor (rad/s)
- *n* : Rotational speed (min⁻¹)

Balance quality grades

The JIS specifies the balance quality grades from G0.4 to G4000. Generally, the three grades described in Table 1 below are commonly used.

Correction of the unbalance of drive shafts

JTEKT corrects the unbalance of drive shafts to the optimal value by the two plane balancing method, using the latest balance system.

To correct the balance of a drive shaft, it is critical to correct the balance between two planes each near the two individual universal joints, instead of by the one plane balancing as used to balance car wheels.

Especially in the case of a long drive shaft, this two plane balancing method is the only way to acquire good results.

Table 1 Recommended balance quality grades (excerpt from JIS B 0905)

Balance quality grade	Upper limit value of balance quality $(e \omega)$	Recommended applicable machines
G40	40	Car wheels, wheel rims, wheel sets and drive shafts Crankshaft systems of elastically mounted high speed four stroke engines (gasoline or diesel) with six or more cylinders Crankshaft systems of the engines of automobiles, trucks and rolling stock
G16	16	Drive shafts with special requirements (propeller shafts and diesel shafts) Components of crushing machines Components of agricultural machines Components of the engines of automobiles, trucks and rolling stock (gasoline or diesel) Crankshaft systems with six or more cylinders with special requirements
G 6.3	6.3	Devices of processing plants Ship engine turbine gears (for merchant ships) Centrifugal drums Papermaking rolls and printing rolls Fans Assembled aerial gas turbine rollers Flywheels Pump impellers Components of machine tools and general industrial machines Medium or large electric armatures (of electric motors having at least 80 mm in the shaft center height) without special requirements Small electric armatures used in vibration insensitive applications and/or provided with vibration insulation (mainly mass produced models) Components of engines with special requirements

Composition of identification numbers





Torque capacity

Model No.	Torque capacity (N·m)			Model No.	Torque capacity (N·m)		
woder no.	Rated $T_{\rm R}$	Normal maximum $T_{ m D}$	Emergency maximum $T_{ m S}$	woder no.	Rated $T_{\rm R}$	Normal maximum $T_{ m D}$	Emergency maximum $T_{\rm S}$
4	466	1 280	3 310	8.5	2 570	7 520	13 500
5	851	1 770	4 470	9	3 450	9 980	18 900
6	1 090	2 240	6 400	10	5 580	13 600	38 900
7	1 650	3 760	9 190	12	8 060	19 300	47 400
8	2 200	5 380	12 200				—

Recommended dimensions of coupling yokes



Model		Boundary dimensions (mm)									
No.	Dc	С		t		holes d					
										Metric screw thread	Unified screw thread
4	114.3	107.93 ^{+0.05} 0	70	3.2	9.5 ^{+0.05}	$3.5 \begin{array}{c} +0.5 \\ 0 \end{array}$	43.63	18.24	11.8	M 8×1.25	5/16-24UNF
5	121.4	115.06 ^{+0.05}	70	4	14.26 +0.05 0	4.9 ^{+0.5} ₀	44.45	21.43	12.6	M10×1.25	3/8-24UNF
6	148.4	140.46 ^{+0.05}	90	4	14.26 +0.05 0	4.9 ^{+0.5} ₀	57.15	21.43	12.6	MIU × 1.25	3/6-24UNF
7	158	148.38 ^{+0.05}	92	4.8	15.85 ^{+0.05}	5.7 ^{+0.5} ₀	58.73	24.61	15.8		
8	215.9	206.32 ^{+0.05}	150	4.8	15.85 ^{+0.05}	5.7 ^{+0.5} ₀	87.3	24.61	17.4	M12×1.25	1/2-20UNF
8.5	174.6	165.07 ^{+0.05}	96	4.8	15.85 ^{+0.05}	5.7 ^{+0.5} ₀	61.91	35.72	19	- MIZA 1.23	
9	219.1	209.52 ^{+0.05}	135	4.8	15.85 ^{+0.05}	5.7 ^{+0.5} ₀	84.14	35.72	19		
10	225.4	212.699 +0.051 0	141	6.4	25.35 +0.07 0	9.3 ^{+0.5} ₀	82.55	46.05	30	- M14×1.5	
12	301.6	288.90 ^{+0.1}	205	6.4	25.35 +0.07 0	9.3 ^{+0.5} ₀	120.65	46.05	30		



Model No. 4 Block type



Bearing fixing boit					
Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$			
Metric screw thread	M8×1.25	36 - 40			
Unified screw thread	5/16-24UNF	30 - 36			

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces <i>L</i> (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		327 (min.)	45	05	Telescoping type (with tube)
1		277		25	Telescoping type (without tube)
2		*	*	*	Telescoping type (integrated structure on shaft side)
3		*	*	25	Long telescoping type
5		176 (min.)		25	Fixed type (with tube)
5		144		23	Fixed type (without tube)
6		98.4		10	Fixed type (integrated)
	Check with us about *parts as they are of	104.8			(structure)

Remark Check with us about *parts as they are designed individually.

Model No. 4 Mixed type



Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$				
Metric screw thread	M8×1.25	36 - 40				
Unified screw thread	5/16-24UNF	30 - 36				

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces <i>L</i> (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
1	344 (min.)		45	0E	Telescoping type (with tube)
		294	40	25	Telescoping type (without tube)
3		573	240	25	Long telescoping type
5		195 (min.)		25	Fixed type (with tube)
5		145		23	Fixed type (without tube)
		97		12	Fixed type
6		100		15	(integrated structure)
		108.5			, /



Model No. 5 Block type



Туре	Size	Tightening torque $N \cdot m$
Metric screw thread	M10×1.25	71 - 77
Unified screw thread	3/8-24UNF	50 - 60

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		336 (min.)		10	Telescoping type (with tube)
1		288	42		Telescoping type (without tube)
2		263	42	10	Telescoping type (integrated structure on) shaft side
3		*	*	10	Long telescoping type
5		178 (min.)		10	Fixed type (with tube)
5		129.56		10	Fixed type (without tube)
6		112		7	Fixed type (integrated) structure)

Model No. 5 Mixed type



Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$			
Metric screw thread	M10×1.25	71 - 77			
Unified screw thread	3/8-24UNF	50 - 66			

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		364 (min.)	54	25	Telescoping type (with tube)
1		314		23	Telescoping type (without tube)
3		*	*	25	Long telescoping type
5		213 (min.)		25	Fixed type (with tube)
		160		Fixed type (without tube)	
6		105		10	Fixed type (integrated) (structure)

Remark Check with us about *parts as they are designed individually.



Model No. 6 Block type



Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$			
Metric screw thread	M10×1.25	71 - 77			
Unified screw thread	3/8-24UNF	50 - 66			

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
1		369 (min.)	47	25	Telescoping type (with tube)
		319	47	25	Telescoping type (without tube)
2		211	15	20	Telescoping type / integrated \
2		273	35	20	(structure on shaft side)
3		610 (min.)	259	25	Long telescoping type
F		216 (min.)		25	Fixed type (with tube)
5		165.96		20	Fixed type (without tube)
		113		5	Fixed type
6		117.1 120		10	(integrated structure)

Model No. 6 Mixed type



Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		381 (min.)	52		Telescoping type (with tube)
1		413 (min.)	85	25	(with tube)
		289	16	25	-
		332	52		Telescoping type (without tube)
		363	85		
3		615 (min.)	265	25	Long telescoping type
5		227 (min.)		25	Fixed type (with tube)
		176.98		20	Fixed type (without tube)
6		103.88		10	Fixed type (integrated)
	ð	187.98		-	(structure)

71 - 77

50 - 66



Model No. 7 Block type



	•	
Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$
Metric screw thread	M12×1.25	132 - 155
Unified screw thread	1/2-20UNF	95 - 108

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		435 (min.)	65		Telescoping type
1		409	47	20	(with tube)
		385	65	20	Telescoping type
		359	47		(without tube)
2		276	21	18	Telescoping type (integrated)
2		290	27	10	structure on shaft side
3		528 (min.)	160	20	Long telescoping type
5		241 (min.)		20	Fixed type (with tube)
5		187.5		15	Fixed type
		195 212		20	(without tube)
6		123.8		5	Fixed type (integrated) structure)

Model No. 7 Mixed type



Bearing fixing bolt						
Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$				
Metric screw thread	M12×1.25	132 - 155				
Unified screw thread	1/2-20UNF	95 - 108				

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		439 (min.)	65	25	Telescoping type (with tube)
1		389		23	Telescoping type
		365	35		(without tube)
3		520 (min.)	160	25	Long telescoping type
5		230 (min.)		25	Fixed type (with tube)
5		179.32		25 -	Fixed type (without tube)
		140		10	Fixed type
6		200		10	(integrated) structure)





Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		475 (min.)	70	05	Telescoping type (with tube)
1		415	76	25	Telescoping type (without tube)
2		*	*	*	Telescoping type (integrated (structure on shaft side)
3		600 (min.)	190	25	Long telescoping type
5		267 (min.)		25	Fixed type (with tube)
5		210 206.64		23	Fixed type (without tube)

Remark Check with us about *parts as they are designed individually.

Model No. 8.5 Block type



Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$			
Metric screw thread	M12×1.25	132 - 155			
Unified screw thread	1/2-20UNF	149 - 162			

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
		494 (min.)	70		Telescoping type
1		512 (min.)	85	25	(with tube)
		436 70 25	Telescoping type (without tube)		
		305	20	17	Telescoping type / integrated \
2		361	40	17	(structure on shaft side)
3		610 (min.)	190	25	Long telescoping type
_		282 (min.)		25	Fixed type (with tube)
5		241.5	-	17	Fixed type
		231 224		25	(without tube)
\vdash		158.8		23	
6		164		10	Fixed type (integrated)
		172			(structure)





Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
1		543 (min.)	Telescoping type (with tube)		
		483	78	25	Telescoping type (without tube)
2		398	56	25	Telescoping type (integrated structure on shaft side)
3		638 (min.)	180	25	Long telescoping type
5		295 (min.)		25	Fixed type (with tube)
5		235	23	Fixed type (without tube)	
6		158.8		25	Fixed type (integrated) structure)

Model No. 10 Block type



Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$		
Metric screw thread	M14×1.5	206 - 220		

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
1		579 (min.)		25	Telescoping type (with tube)
		509	70		Telescoping type (without tube)
2		489	70	25	Telescoping type (integrated (structure on shaft side)
3		*	*	25	Long telescoping type
5		353 (min.)		25	Fixed type (with tube)
		280 269			Fixed type (without tube)

Remark Check with us about *parts as they are designed individually.



Model No. 12 Block type



M

Туре	Size	Tightening torque $N{\boldsymbol{\cdot}}m$
Metric screw thread	M14×1.5	206 - 220

Structure code	Structure sketch (The red lines indicate welding parts.)	Length between attaching surfaces L (mm)	Allowable telescoping stroke S (mm)	Max operating angle (°)	Features
1		676 (min.)			Telescoping type (with tube)
		606	82	25	Telescoping type (without tube)
2		*	*	*	Telescoping type (integrated (structure on shaft side)
3		*	*	*	Long telescoping type
5		369 (min.)		25	Fixed type (with tube)
		306.3			Fixed type (without tube)

Remark Check with us about *parts as they are designed individually.

Analysis/evaluation equipment 🔘

With improvement with FEM using a 3D model and review of the allowable differential angle based on our achievement in the market over more than 40 years, JTEKT proposes optimal design and products suitable for applications.

We also implement evaluation with actual products as necessary.

Large-sized torsion testing machine

Example of FEM analysis





Example of review of allowable differential angle





Drive shaft selection sheet



	Item		Necessity		Description		Remarks
Name of the machine		0					
Loca	ation of installation		0				
(1)	Size/type		0				
(2)	Torque transmission	(N·m)	O	Normal	Max.	Emergency max.	
(3)	Rotational speed	(min ⁻¹)	0	Normal	Max.		
(4)	Operating angle	(deg)	0	Normal	Max.		
(5)	Required telescoping	(mm)	0				
(6)	Limited swing diameter	(mm)					
(7)	Paint color						Black if not specified
(8)	Ambient temperature	(°C)					
(9)	Special environmental conditions						
(10)	Service life requirement	(h)	0				
(11) Attaching dimension L=(() mm $L=() mm$ $L=() mm$							

TEKT

OFFICES ■

KOYO CANADA INC.

5324 South Service Road, Burilngton, Ontario L7L 5H5, CANADA TEL : 1-905-681-1121 FAX : 1-905-681-1392

JTEKT NORTH AMERICA CORPORATION

-Main Office-

47771 Halyard Drive, Plymouth, MI 48170, U.S.A. TEL : 1-734-454-1500 FAX : 1-734-454-7059

-Cleveland Office-

29570 Clemens Road, P.O.Box 45028, Westlake, OH 44145, U.S.A TEL : 1-440-835-1000 FAX : 1-440-835-9347

KOYO MEXICANA, S.A. DE C.V. Av. Insurgentes Sur 2376-505, Col. Chimalistac, Del. Álvaro Obregón, C.P.01070, México, D.F. TEL : 52-55-5207-3860 FAX : 52-55-5207-3873

KOYO LATIN AMERICA, S.A.

Edificio Banco del Pacifico Planta Baja, Calle Aquilino de la Guardia y Calle 52, Panama, REPUBLICA DE PANAMA TEL : 507-208-5900 FAX : 507-264-2782/507-269-7578

KOYO ROLAMENTOS DO BRASIL LTDA.

Avenida Brigadeiro Faria Lima, 1744 - 1st Floor - CJ.11 São Paulo - SP - Brazil CEP 01451-001 TEL : 55-11-3372-7500 FAX: 55-11-3887-3039

KOYO MIDDLE EAST FZE

6EA 601, Dubai Airport Free Zone, P.O.Box 54816, Dubai, U.A.E. TEL : 97-1-4299-3600 FAX : 97-1-4299-3700

KOYO BEARINGS INDIA PVT. LTD.

C/o Stylus Commercial Services PVT LTD, Ground Floor, The Beech, E-1, Manyata Embassy Business Park, Outer Ring Road, Bengaluru-560045, INDIA TEL : 91-80-4276-4567 (Reception Desk of Service Office) FAX : 91-80-4276-4568

JTEKT (THAILAND) CO., LTD.

172/1 Moo 12 Tambol Bangwua, Amphur Bangpakong, Chachoengsao 24180, THAILAND TEL : 66-38-533-310~7 FAX : 66-38-532-776

PT. JTEKT INDONESIA

JI. Surya Madya Plot I-27b, Kawasan Industri Surya Cipta, Kutanegara, Ciampel, Karawang Jawa Barat, 41363 INDONESIA TEL : 62-267-8610-270 FAX : 62-267-8610-271

KOYO SINGAPORE BEARING (PTE.) LTD.

27, Penjuru Lane, Level 5, Phase 1 Warehouse #05-01. SINGAPORE 609195 TEL: 65-6274-2200 FAX: 65-6862-1623

PHILIPPINE KOYO BEARING CORPORATION

6th Floor, One World Square Building, #10 Upper McKinley Road, McKinley Town Center Fort Bonifacio, 1634 Taguig City, PHILIPPINES TEL : 63-2-856-5046/5047 FAX : 63-2-856-5045

JTEKT KOREA CO., LTD.

Seong-do Bldg 13F, 207, Dosan-Dearo, Gangnam-Gu, Seoul, KOREA TEL : 82-2-549-7922 FAX : 82-2-549-7923

JTEKT (CHINA) CO., LTD.

Room 25A2, V-CAPITAL Building, 333 Xianxia Road, Changning District, Shanghai 200336, CHINA TEL : 86-21-5178-1000 FAX : 86-21-5178-1008

KOYO AUSTRALIA PTY. LTD.

Unit 2, 8 Hill Road, Homebush Bay, NSW 2127, AUSTRALIA TEL : 61-2-8719-5300 FAX : 61-2-8719-5333

JTEKT EUROPE BEARINGS B.V.

Markerkant 13-01, 1314 AL Almere, THE NETHERLANDS TEL : 31-36-5383333 FAX : 31-36-5347212

-Benelux Branch Office-

Energieweg 10a, 2964 LE, Groot-Ammers, THE NETHERLANDS TEL : 31-184-606800 FAX : 31-184-606857

-Sosnowiec Branch Office-

ul3 Maja14, 41-200 Sosnowiec, POLAND TEL : 48-32-720-1444 FAX : 48-32-746-7746

KOYO KULLAGER SCANDINAVIA A.B. Johanneslundsvägen 4, 194 61 Upplands Väsby, SWEDEN TEL : 46-8-594-212-10 FAX : 46-8-594-212-29

KOYO (U.K.) LIMITED

Whitehall Avenue, Kingston, Milton Keynes MK10 0AX, UNITED KINGDOM TEL : 44-1908-289300 FAX : 44-1908-289333

KOYO DEUTSCHLAND GMBH

Bargkoppelweg 4, D-22145 Hamburg, GERMANY TEL : 49-40-67-9090-0 FAX : 49-40-67-9203-0

KOYO FRANCE S.A.

6 Avenue du Marais BP20189, 95105 Argenteuil Cedex, FRANCE TEL : 33-1-3998-4202 FAX : 33-1-3998-4244/4249

KOYO IBERICA, S.L.

Avda. de la Industria, 52-2 izda 28820 Coslada Madrid, SPAIN TEL : 34-91-329-0818 FAX : 34-91-747-1194

KOYO ITALIA S.R.L.

Via Stephenson 43/a 20157 Milano, ITALY TEL: 39-02-2951-0844 FAX: 39-02-2951-0954

-Romanian Representative Office-

24, Lister Street, ap. 1, sector 5, Bucharest, ROMANIA TEL : 40-21-410-4182 FAX : 40-21-410-1178

PUBLISHER

JTEKT CORPORATION NAGOYA HEAD OFFICE No.7-1, Meieki 4-chome, Nakamura-ku, Nagoya, Aichi 450-8515, JAPAN ———————————————————————————————————	FAX : 81-52-527-1911
JTEKT CORPORATION OSAKA HEAD OFFICE No.5-8, Minamisemba 3-chome, Chuo-ku, Osaka 542-8502, JAPAN	FAX : 81-6-6245-3712
Sales & Marketing Headquarters No.5-8, Minamisemba 3-chome, Chuo-ku, Osaka 542-8502, JAPAN ———————————————————————————————————	FAX : 81-6-6244-9007

 \ddagger The contents of this catalog are subject to change without prior notice. Every possible effort has been made to ensure that the data herein is correct; however, JTEKT connot assume responsibility for any errors or omissions.

Reproduction of this catalog without written consent is strictly prohibited.

Koyo, High Wing Series Drive Shafts



CAT.NO.B2022E Printed in Japan '16.01-1CM